

PHASE FORMATION IN THE Tb-Co-Cu SYSTEM IN A RANGE OF Tb₃(Co,Cu) COMPOUND

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Abstract

In recent years, the application of various additions (hydrides, oxides, intermetallic compounds, etc.) in powder mixtures for manufacturing Nd-Fe-B magnets shows promise as the method that allows one to increase the hysteretic characteristics of the magnets at the expense of realized grain-boundary diffusion and grain-boundary structuring processes. The processes allow one to introduce both the heavy rare-earth metals and copper that was shown also to favour the increase in the hysteretic parameter of Nd-Fe-B-based compositions. In the present work, we consider the alloys $Tb_3(Co_{1-x},Cu_x)$ with $x = \sim 0.4$ as additions to Nd-Fe-B-based powder mixtures. The alloys were prepared by arc melting in an argon atmosphere and subjected to homogenizing annealing at 600 °C for 90 h. The phase composition and phase equilibria in the system were studied by X-ray diffraction analysis, differential thermal analysis (DTA), optical and scanning electron microscopy, electron microprobe analysis, and low-temperature thermal magnetic analysis. The composition was shown to be three-phase, $Tb_3(Co,Cu)$, $Tb_{12}(Co,Cu)_7$, and Tb(Co,Cu) that is the primarily solidified phase in the system. The copper solubility in the Tb_3Co and $Tb_{12}Co_7$ compounds and cobalt solubility in the TbCu compound were determined. A portion of the isothermal section of the Tb-Co-Cu system with at 600 °C was constructed. The possibility of the hydrogenation of the $Tb_3(Co_{1-x},Cu_x)$ composition with $x = \sim 0.4$ with the formation of TbH_x , Co, Cu was demonstrated.

Keywords: Grain boundary diffusion, Nd-Fe-B magnets, Tb-Co-Cu system, phase equilibria

1. INTRODUCTION

Recently, the significant increase in the hysteretic properties of the sintered Nd-Fe-B-based magnets has been demonstrated in using additions of rare-earth metal (REM) compounds (hydrides, fluorides, oxides, intermetallides and low-melting eutectics). The increase is reached at the expense of grain-boundary diffusion of heavy REM with the formation of (Nd, R)₂Fe₁₄B "shells" at grain boundaries of the main magnetic phase and subsequent grain boundary restructuring [1-10]. The use of R₃Co compounds (R = Nd, Dy) was realized in [11] by introducing them into permanent magnets through the gas phase and led to the increase in the hysteretic properties, namely, in the coercive force from 400 to 875 kA/m.

Earlier, we have showed the application of hydrogenated $R_3(Co, Cu)$ compounds as additions to Nd-Fe-B powder mixtures in order to increase the hysteretic properties of magnets [12]. The use of hydrogenated Cu-



containing REM compounds is described in [13] and also demonstrated an extreme increase in the hysteretic characteristics of Dy-depleted magnets owing to the introduction of Cu. The use of compounds containing Co and Cu simultaneously can solve the problem of introducing these components into the magnet composition. It is known that the alloying with cobalt leads to an increase in the Curie temperature of compound REM₂(Fe, Co)₁₄B [14], and also allows the temperature coefficient of induction to be regulated. Thus, the introduction of cobalt and copper into the alloy can favor the reaching of required level of hysteretic properties of magnets.

All REM-rich R_3 Co compounds are formed by a peritectic reaction [15] and thus their preparation in a single-phase state is difficult. Phase equilibria in R-Co-Cu systems, in particular, with REM contents of 67-75 at. % have not yet been adequately studied [16]. The concentration limits of the existence of R_{12} (Co, Cu)₇, R_3 (Co, Cu) and R(Cu, Co) ternary phases [17] have not been determined. These data are of importance in understanding processes occurred during saturation of alloys with hydrogen in manufacturing of magnets. The R_3 Co compounds have an orthorhombic structure of the Fe_3 C type (the Pnma space group) [18].

The present work is devoted to the study of phase equilibria of the Tb-Co-Cu system in the concentration range of Tb 60-100 at.%. The interaction of the $Tb_3(Co_{1-x}Cu_x)$ alloy with hydrogen is also considered in order to predict the behavior of $Tb_3(Co_{1-x}Cu_x)$ additions in manufacturing of Nd-Fe-B-based permanent magnets.

2. EXPERIMENTAL

The $Tb_3(Co_{1-x}Cu_x)$ alloy with x = 0.4 was prepared by arc melting of starting components (Tb-99.9 at.%, electrolytic Co K-1 grade, and oxygen-free copper) in an argon atmosphere using a water-cold copper mould and a nonconsumable tungsten electrode. The ingot was subjected to homogenizing annealing at 600 °C for 90 h followed by rapid cooling (20°C/min); thus fixed phase state corresponds to a temperature of 600 °C. The structure of the alloy was studied by optical and electron microscopy using an AxioLabA1 (Carl Zeiss) microscope and a QUANTA 450 FEG electron microscope equipped with an EDX APOLLO X microanalyzer, respectively; the back-scattered electron (BSE) mode image was used. The magnetic properties of the alloy were measured in the temperature range of 4.2-300 K in a magnetic field of 100 Oe using a vibrating-sample magnetometer and an NM-1 Oxford superconducting magnet. The differential thermal analysis of the alloy was carried out in an argon atmosphere at a heating/cooling rate of 15°C/min using a Setaram Setsys -1750 device. The Tb-Co-Cu alloy was saturated with hydrogen at 270°C in a hydrogen flow (at 0.1 MPa pressure) for 1 h. The phase composition of the alloy was studied by X-ray diffraction (XRD) analysis using a Ultima IV (Rigaku, Japan) diffractometer equipped with a "D/teX" detector, CuKα radiation; the scanning step is 0.001°). X-ray diffraction patterns were process and the phase composition of alloys was determined using PowderCell software. The data on the crystal structure type, lattice parameters, and crystallographic positions of atoms in the Tb-Co, Tb-Cu, and H-Tb system alloys were used to simulate theoretical XRD patterns [19-21].

3. RESULTS AND DISCUSSION

3.1. Microstructure and electron microprobe analysis of Tb₃(Co,Cu) alloy

The microstructure of $Tb_3(Co,Cu)$ alloy subjected to prolonged homogenizing annealing is shown in **Figure 1**. As is seen, the structure is not single-phase and is characterized by the presence of rounded and petal-shaped inclusions. The element composition of the observed inclusions in the $Tb_3(Co,Cu)$ alloy was determined by SEM/EDX method (**Table 1**). According to EMA data, the compositions of inclusions correspond to $Tb_3(Co, Cu)$ (main phase); Tb(Cu, Co) (large inclusions), and of $Tb_{12}(Co, Cu)_7$ (small inclusions) (see **Figure 1b**).



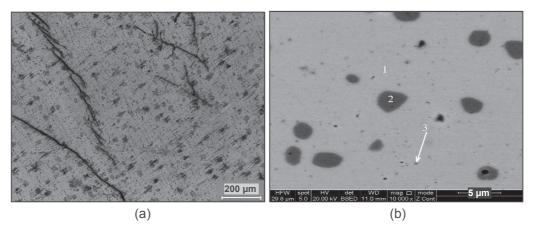


Figure 1 (a) Microstructure of Tb₃(Co,Cu) alloy after homogenizing annealing (optical microscopy) and (b) SEM (BSE) image of the structure: 1 - Tb₃(Co,Cu), 2 - Tb(Co,Cu), 3 - Tb₁₂(Co,Cu)

Thus, the alloy subjected to prolonged homogenizing annealing is multiphase. The determined limits of Co / Cu solubility in the found phases correspond to compositions $Tb_3(Co_{1-x}Cu_x)$ with x = 0.25-0.27; $Tb(Cu_{1-y}Co_y)$ with y = 0.05-0.19, and $Tb_{12}(Co_{1-z}Cu_z)$ with z = 0.4.

Table 1 Electron microprobe analysis data for the Tb₃(Co,Cu) alloy (at.%)

Element/phase	Tb	Со	Cu	
Phase_1	55.1	8.1	36.8	
Phase_2	74.6	18.8	6.6	
Phase_3	68.0	19.2	12.8	

3.2. X-ray diffraction analysis

Figure 3 shows X-ray diffraction analysis of the alloy $Tb_3(Co,Cu)$ subjected to prolonged annealing in an argon atmosphere. To identify observed reflections, the X-ray diffraction pattern was processed using PowderCell software. Unmarked reflections (in **Figure 2**) belong to the main $Tb_3(Co,Cu)$ phase; marked reflections correspond to $Tb(Cu_{1-y}Co_y)$ and $Tb_{12}(Co_{1-z}Cu_z)$ phases. The analysis of crystal structures of the found compounds and construction of theoretical XRD patterns for the simulated structures allowed us to determine variations of lattice parameters of phases alloyed with Co (for $Tb(Cu_{1-y}Co_y)$) and Cu (for $Tb_3(Co_{1-x}Cu_x)$) and $Tb_{12}(Co_{1-z}Cu_z)$ (see **Table 2**). As is seen, the alloying of the binary compounds with Co and Cu does not change the crystal structure type of binary compounds. The phases present in the alloy are alloyed modifications of the binary compounds in accordance with their phase diagrams [15, 17].

Table 2 Crystallographic parameters of the Tb-Co-Cu phases for a composition range of Tb 60-75 at.%

Nº	Compound	Space group	С	a (nm)	b (nm)	c (nm)	References
1	Tb₃Co	Pnma	Fe ₃ C	0.6985	0.9380	0.6250	[18]
2	Tb ₃ (Co _{1-x} Cu _x), x=0.25-0.27	Pnma	Fe ₃ C	0.69723	0.94343	0.62623	This work
3	Tb ₁₂ Co ₇	P2 ₁ /c	H012C07	0.8390	0.1132	0.1397	[21]
4	Tb ₁₂ (Co _{1-z} Cu) ₇ z=0.4	P2 ₁ /c	Ho ₁₂ Co ₇	0.829	0.1122	0.1387	This work
5	TbCu	Pm3m	CsCl	3.48	3.48	3.48	[20]
6	Tb(Cu _{1-y} Co _y) y=0.05-0.19	Pm3m	CsCl	3.4791	3.4791	3.4791	This work



X-ray diffraction data confirmed the presence of the phase following phases found by EMA: Tb₃Co, Tb₁₂Co₇, TbCu. Analysis of variations of the lattice parameters indicates the alloying of the present phases with cobalt and copper with varying degrees of substitution of Cu for Co and of Co for Cu.

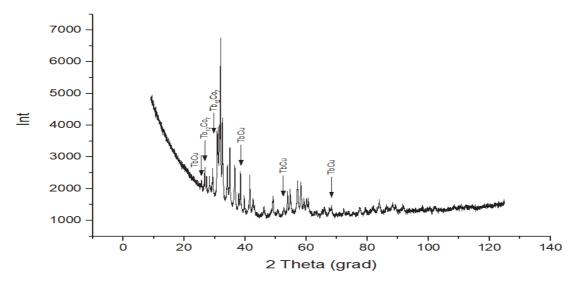


Figure 2 X-ray diffraction pattern of the Tb₃(Co,Cu) alloy

3.3. Magnetic measurements

The temperature dependence of the magnetization of compound $Tb_3(Co,Cu)$ in a weak magnetic field in a temperature range 4.2-250 K (**Figure 3**) was measured and analyzed. It is known [18] that the compound Tb_3Co demonstrates the paramagnetic-antiferromagnet transformation at $T_N = 82$ K and a metamagnetic transformation at $T_N = 82$ K related to the incommensurability of the magnetic and crystal structures. These transformations are clearly observed in the dependence (anomalies 1 and 2, respectively).

The analysis of the measured curve given in Figure 3 allows us to determine the temperatures of the phase

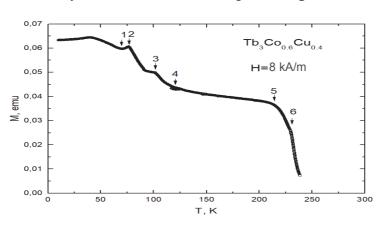


Figure 3 The temperature dependence of the magnetization of $Tb_3(Co_{1-x}Cu_x)$ alloy with x = 0.4 measured in a magnetic field of 8 kA/m

transitions corresponding to change in the magnetic order of the compounds: Curie temperature of the Tb₁₂(Co,Cu)₇ compound is T_C = 100 K (3), the Neel temperature of the Tb(Co,Cu) compound is $T_N = 115 \text{ K}$ (4), and the Neel and Curie temperature of Tb equal to $T_N = 218 \text{ K}$ (5) and $T_C = 230 \text{ K}$ (6), respectively. The determined temperatures of the phase transitions agree adequately with data obtained by other investigators [22-24]. As discussed above, the alloy has the multiphase composition. Moreover, the measurements allowed us to identify the presence of pure Tb. Thus, we can conclude that the fixed state of the alloy Tb₃(Co_{1-x}Cu_x) with x = 0.4 is nonequilibrium.

3.4. Phase equilibria in the Tb-Co-Cu system

The Tb₃(Co, Cu) alloy was studied by the DTA during heating and cooling. According to the DTA data (**Figure 4**), the solidification of the alloy begins with the precipitation of primary crystals of Tb(Co, Cu)



compound at a temperature of temperature ~770 °C, corresponding to equilibrium L + Tb(Co,Cu)_{primary} (solidus). At a temperature of ~732 °C, a peritectic reaction occurs with the formation of Tb₃(Co,Cu), equilibrium L + Tb(Co,Cu)_{primary} + Tb₃(Co,Cu). At a temperature of ~663 °C, the Tb₁₂(Co, Cu)₇ phase is formed by the peritectic reaction; equilibrium L + Tb₃(Co,Cu) + Tb(Co,Cu)_{primary} + Tb₁₂(Co,Cu)₇.

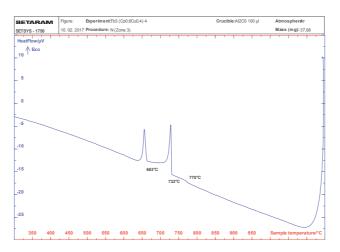


Figure 4 The temperature dependence of the magnetization of $Tb_3(Co_{1-x}Cu_x)$ alloy with x = 0.4 measured in a magnetic field of 8 kA/m

Based on the XRD and EMA data (SEM/EDX) and magnetic measurements, and DTA data, a portion of isothermal section of the Tb-Co-Cu ternary system at a temperature of 600 ° C was constructed for a composition range of Tb 60-100% (**Figure 5**) and a solidification scheme for the alloy was proposed. The alloy under study is marked by a "cross" in the region of existence of three-phase equilibrium: Tb + Tb₃Co + Tb₁₂Co₇.

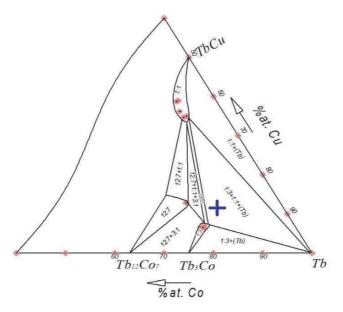


Figure 5 Isothermal section of the Tb-Co-Cu ternary system at 600 °C

3.5. Interaction of Tb₃(Co_{1-x}Cu_x) alloy with hydrogen

Saturation of the alloy $Tb_3(Co, Cu)$ with hydrogen led to the embrittlement of the alloy, preparation of a powder material suitable for the further introduction of the composition into the Nd-Fe-B magnetic alloy powder during cooperative mailing. After saturation with hydrogen, the alloy was studied by XRD (**Figure 6**, unmarked reflections correspond to TbH_2 hydride).



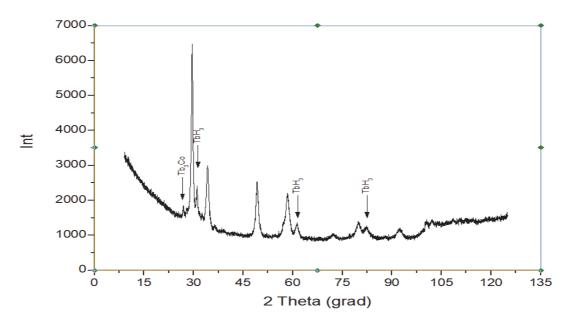


Figure 6 X-ray diffraction pattern of the alloy Tb₃(Co,Cu) after saturation with hydrogen

As is seen, the saturation of the alloy with hydrogen leads to the formation of terbium hydrides TbH₂ and TbH₃, a small amount of the Tb₃(Co,Cu) also is present. Simulation of X-ray diffraction patterns of Co, Cu and Tb₁₂(Co,Cu) and Tb(Co,Cu) phases did not allowed us to find the presence of the phases in the hydrogenated alloy. We assume the presence of a finely dispersed mixture (Co, Cu) without the formation of a quasi-solid solution.

4. CONCLUSION

- The microstructure of the alloy Tb₃(Co,Cu) was studied by optical and electron microscopy. The EMA allowed us to determine the compositions of the present phases. The concentration limits of Co / Cu solubilities in the phases are determined.
- X-ray diffraction analysis of the alloy carried out in using PowderCell software indicated the presence of the Tb₃(Co, Cu), Tb (Co, Cu) and Tb₁₂(Co, Cu)₇ phases and confirmed the existence of solubility of Cu and Cu corresponding phases.
- The temperature dependence of the magnetization of the Tb₃(Co,Cu) alloy was studied in the temperature range 4.2-300 K. The magnetic measurements allowed us to find the presence of Tb in the alloy. The temperatures of magnetic transformations of the present phases were observed in the dependence.
- The isothermal section of the ternary Tb-Co-Cu system at 600 ° C was constructed. The solidification path of the studied alloy was described using DTA data.
- Saturation of the alloy with hydrogen leads to the embrittlement of composition with the formation of mainly TbH₂ TbH₃ hydrides; a small amount of residual Tb₃(Co, Cu) compound is observed.

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